A Simplified Formulation for the Backward/Forward Sweep Power Flow Method

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Abstract

This paper describes a simplified formulation of the Backward/Forward (BW/FW) Sweep Power Flow applied to radial distribution systems with distributed generation under positive sequence modelling. Proposed formulation was applied in an illustrative test system.

Keywords: Backward/forward sweep, load flow, power flow, distribution system analysis

1 Introduction

Several Backward/Forward (BW/FW) sweep algorithms have been discussed in literature. In 1967, Berg presented a paper which can be considered as the source for the all variants of BW/FW sweep methods [1]. Later, a similar approach was presented in [2] based on ladder network theory. The BW/FW Sweep algorithms use the Kirchhoff laws. Different formulations can be found [3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 15, 14]. BW/FW sweep methods typically present a slow convergence rate but computationally efficient at each iteration. Using these methods, power flow solution for a distribution network can be obtained without solving any set of simultaneous equations. In this work, the standard BW/FW sweep power flow is reformulated in convenient form. An illustrative four-bus example is solved.

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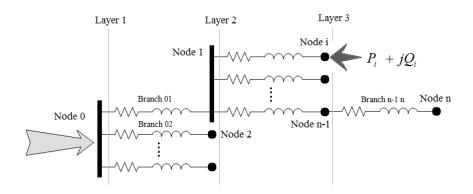


Figure 1: Branch and node numbering of a radial distribution network

2 The Method

The input data of this algorithm is given by node-branch oriented data used by most utilities. Basic data required is: active and reactive powers, nomenclature for sending and receiving nodes, and positive sequence impedance model for all branches.

In the following, the standard BW/FW sweep power flow method is written in matrix notation using complex variables. Branch impedances are stated as a vector \mathbf{Z} corresponding to a distribution line model containing a series positive sequence impedance for line or transformer. Shunt impedances are not considered in this first approach. Fig. 1 shows a radial distribution network with n+1 nodes, and n branches and a single voltage source at the root node 0. Branches are organized according to an appropriate numbering scheme (list), which details are provided in [3].

$$\mathbf{Z} = \begin{bmatrix} \overline{Z}_{01} & \dots & \overline{Z}_{ij} & \dots & \overline{Z}_{mn} \end{bmatrix}$$
 (1)

where,

$$\overline{Z}_{ij} = R_{ij} + jX_{ij} \quad i, j = 1, ..., n \quad i \neq j$$
(2)

Bus data is given by

$$\mathbf{S} = \begin{bmatrix} \overline{S}_1 \\ \vdots \\ \overline{S}_i \\ \vdots \\ \overline{S}_n \end{bmatrix} = \begin{bmatrix} P_1 + jQ_1 \\ \vdots \\ P_i + jQ_i \\ \vdots \\ P_n + jQ_n \end{bmatrix}$$

$$(3)$$

where net nodal active and reactive powers are given by generated and demanded powers:

$$P_i = P_{Gi} - P_{Di} \tag{4}$$

$$Q_i = Q_{Gi} - Q_{Di} \tag{5}$$

The numbering of branches in one layer begins only after all the branches in the previous layer have been numbered. Considering that initial voltages are known: voltage at substation is set $\overline{V}_0 = Vref$ and an initial voltage vector is given by:

$$\mathbf{V}^0 = \left[\begin{array}{cccc} \overline{V}_1^0 & \dots & \overline{V}_i^0 & \dots & \overline{V}_n^0 \end{array} \right] \tag{6}$$

The state of the system is reached solving two steps iteratively.

2.1 Step 1 - Backward Sweep

For each iteration k, branch currents are aggregated from loads to origin:

$$\mathbf{J}^{\mathbf{k}} = -\mathbf{T} \cdot \mathbf{I}^{\mathbf{k}} \tag{7}$$

The relationship between nodal currents $\mathbf{I}^{\mathbf{k}}$ and branch currents $\mathbf{J}^{\mathbf{k}}$ is set through an upper triangular matrix \mathbf{T} accomplishing the Kirchhoff Current Laws (KCL). Each element \overline{I}_i^k of $\mathbf{I}^{\mathbf{k}}$ associated to node i is calculated as function of injected powers \overline{S}_i and its voltage profile \overline{V}_i^k as shown below:

$$\overline{I}_i^k = \frac{\overline{S}_i^*}{\overline{V}_i^{k*}} \quad i = 1, ..., n \tag{8}$$

2.2 Step 2 - Forward Sweep

Nodal voltage vector \mathbf{V} is updated from the origin to loads according the Kirchhoff Voltage Laws (KVL), using previously calculated branch currents vector \mathbf{J} , branch impedances vector \mathbf{Z} :

$$\mathbf{V}^{k+1} = \mathbf{V}_0 - \mathbf{T}^T \cdot \mathbf{D}_{\mathbf{Z}} \cdot \mathbf{J}^k \tag{9}$$

where V_0 is a *n*-elements vector with all entries set at voltage at origin (swing node) \overline{V}_0 and branch impedances $\mathbf{D}_{\mathbf{Z}}$ is the diagonal matrix of vector \mathbf{Z} :

Using Eq. 7

$$\mathbf{V}^{k+1} = \mathbf{V}_0 + \mathbf{T}^T \cdot \mathbf{D}_{\mathbf{Z}} \cdot \mathbf{T} \cdot \mathbf{I}^{\mathbf{k}}$$
(10)

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Updated voltages can be updated using only one equation:

$$\mathbf{V}^{k+1} = \mathbf{V}_0 + \mathbf{TRX} \cdot \mathbf{I}^{\mathbf{k}} \tag{11}$$

where $\mathbf{TRX} = \mathbf{T}^T \cdot \mathbf{D_Z} \cdot \mathbf{T}$

2.3 Convergence

Updated voltages are compared with previous voltages in order to perform convergence check in.

$$\varepsilon \le |\overline{V}_i^{k+1} - \overline{V}_i^k| \quad i = 1, ..., n \tag{12}$$

3 Illustrative Example: Simply 4-node Network

To illustrate the proposed methodology, it is used the 4-node example shown in Fig. 2. Length of all sections is 1 mile. Load demand at nodes 2 and 3 are 2MW with $\cos \varphi = 1.0$.

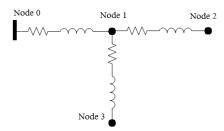


Figure 2: 4-Node Network Topology

Using the following bases $S_B = 10$ MW and $V_B = 12.47$ kV, data and results are given in per unit. Loads are 0.2 in nodes 2 and 3. Reference voltage at node 0 is $\overline{V}_0 = 1 + j0$ and initial voltages are set $\mathbf{V}^0 = \begin{bmatrix} 1 + 0j & 1 + 0j & 1 + 0j \end{bmatrix}$.

Branches are represented by:

$$\mathbf{Z} = \mathbf{R} + j\mathbf{X} = \begin{bmatrix} .0296 \\ .0296 \\ .0296 \end{bmatrix} + j \begin{bmatrix} .0683 \\ .0683 \\ .0683 \end{bmatrix}$$

Network topology is represented through a 3x3 upper triangular matrix **T**.

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$$\mathbf{T} = \left[\begin{array}{ccc} 1 & 1 & 1 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{array} \right]$$

Then, $\mathbf{D}_{\mathbf{Z}}$ is:

$$\mathbf{D_Z} = \left[\begin{array}{ccc} .0296 + j.0683 & .0 & 0 \\ 0 & .0296 + j.0683 & 0 \\ 0 & 0 & .0296 + j.0683 \end{array} \right]$$

Solution reached at iteration 3 for $\varepsilon = 10^{-4}$ and displayed in Table 1. Results are presented in per unit and degrees.

Table 1: 4 Node State of the System - balanced Approach

V_0	$ heta_0$	V_1	$ heta_1$	V_2	$ heta_2$	V_3	θ_3
1.000	0.00	0.987	-1.59	0.981	-2.40	0.981	-2.40

4 Conclusion

This paper describes a convenient formulation of the Backward/Forward (BW/FW) Sweep Power Flow applied to radial distribution systems with distributed generation. Proposed formulation was applied in an illustrative test system.

5 Nomencalture

List of Symbols

 $\mathbf{D}_{\mathbf{Z}}$ Diagonal matrix of branch impedance vector \mathbf{Z}

R Diagonal matrix of branch resistance vector $\Re e \mathbf{Z}$

 ${f X}$ Diagonal matrix of branch reactance vector $Im{f Z}$

 ε Convergence criteria

I Current vector

J Branch Current vector J

n Number of nodes, excluding origin

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- P Active Power Injected vector
- **Q** Reactive Power Injected vector
- P_j Active Power Injected at node j
- Q_j Reactive Power Injected at node j
- P_{Dj} Active Power Demanded at node j
- Q_{Di} Reactive Power Demanded at node j
- P_{Gi} Active Power Generated at node j
- Q_{Gj} Active Power Generated at node j
- R_{ij} Resistance between node i and node j
- S_{Di} Apparent Power Demanded at node j
- S_{Gj} Apparent Power Generated at node j
- T Triangular matrix
- V Voltage vector
- X_{ij} Reactance between node i and node j
- **Z** Branch Impedance vector **Z**
- \overline{Z}^{ij} Branch Impedance between node i and node j
- \mathbf{Z}^{ij} Impedance matrix between node i and node j

Operators

- T Transpose Matrix
- D Diagonal Matrix
- * Conjugate of a complex number

Sub-Indexes

- i Associated to node i
- j Associated to node j
- k Associated to iteration k

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