# Rescue Craft Allocation in Tidal Waters of the North and Baltic Sea

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#### Abstract

This paper aims to improve the average response time for naval accidents in the North and Baltic Sea. To do this we optimize the strategic distribution of the vessel fleet used by the Deutsche Gesellschaft zur Rettung Schiffbrüchiger (German Maritime Search and Rescue Service) (DGzRS) across several home stations. Based on these locations, in case of an incoming distress call the vessel with the lowest response time is dispatched. A particularity of the region considered is the fact that due to low tide, at predictable times some vessels and stations are not operational. In our work, we build a corresponding mathematical model for the allocation of rescue crafts to multiple stations. Thereafter, we show that the problem is  $\mathcal{NP}$ -hard. Next, we provide an Integer Programming (IP) formulation. Finally, we propose several methods of simplifying the model and do a case study to compare their effectiveness. For this, we generate test instances based on real-world data.

*Keywords:* Search and Rescue, Tides, Rescue Craft Allocation, Maritime, Integer Programming, Facility Location

# 1. Introduction

The water territory of Germany is home to a multitude of maritime traffic. These ships transporting both people and goods are exposed to a variety of dangers, ranging from human error to extreme weather, all of which may lead to the necessity of calling for external aid. For the water territory of Germany, the DGzRS is primarily responsible for delivering aid [1]. In 2022 alone, over 2000 instances of vessels in need of assistance were recorded [2].

Oftentimes, the speed at which an adequate rescue vessel arrives can make a difference between life and death, see [3]. Thus, ensuring a timely arrival of rescue crafts is an important factor to maritime safety. The following work uses mathematical optimization of vessel locations to reduce average arrival times, and thereby contribute to saving lives. This is done by focusing on the strategic decision made by the DGzRS of where to place the vessels of their fleet to ensure the fastest possible average response time for future incidents.

The rescue process, as far as it is relevant to our work, is the following: A ship somewhere near the German coastline suffers an accident that necessitates help from outside forces. It then calls the control center of the DGzRS and details both its position and type of incident. The control center in return checks the list of their available response vessels and decides which of them to send. This vessel is then deployed to help the ship with the incident.

Thus, the Rescue Craft Allocation Problem (RCAP) consists of allocating a set of different vessel types to stations in order to ensure minimal response times to maritime incidents, given a region consisting of zones in which incidents occur as well as stations at fixed positions. This is hindered by the fact that each station can only house specific types of crafts as well as that at (predictable) times some stations are inoperable due to the tides. Furthermore, some regions are more incident-prone and require more attention than others.

Additionally, since the DGzRS boats are manned by volunteers, each harbor has to house a single rescue craft. For example, the harbour of Juist dries up twice a day. During that time, the region their station normally covers needs to be covered by the neighbouring stations. This makes it less desirable to position the fastest vessel available there. However we can not permanently place the station from Juist elsewhere since the crew of the ship consists of volunteers living on the island, who can not be resettled.

This works contributions are twofold. First, it is novel insofar as, to the best of our knowledge, there have been not previous attempts to use mathematical optimization for search-and-rescue craft allocation in either the North or the Baltic Sea. Second, the consideration of tides is a novel attribute that specifically matters in seas with a large tidal range, e.g., the North and Baltic Seas. Additionally, we provide a working implementation of our solution algorithms and the corresponding data.

The remainder of the paper is structured as follows: in Section 2 we introduce the RCAP and give a brief overview of related works. Past this, in Section 3 we formally introduce the RCAP. Afterward, in Section 4, we prove that RCAP is  $\mathcal{NP}$ -hard and examine why. In Section 5, we formulate the RCAP as an Integer Program (IP) and we consider simplifications with the aim of reducing computation times with minimal precision losses. Having done this, in Section 6 we conduct a case study on the effect of these simplifications across several test instances. We discuss the results in Section 7, and summarize our findings and give avenues for further research in Section 8.

# 2. Related Work

In the following, we discuss research that includes optimization of search and rescue vessel locations.

The motivation driving our work is also the basis of [4] in which the aim is to find suitable criteria to find the optimal placement of a single rescue vessel. To the best of our knowledge, [4] is also the first paper to address the problem rescue vessel placement. The problem of optimal assignment of a single craft can also be found in [5] which places greater focus on the size and form of the zones generated as well as transforming the historical numbers of incidents into probabilistic values. In comparison, [6] do not limit themselves to placement of a single vessel. However, they make the same assumption as us that only a single vessel is assigned to each harbour. They then solve the problem through a multistage approach based on k-means and natureinspired heuristics. At the same time, their problem strongly differs from the one in this work, as it focuses on dynamic duty points at sea.

Another similar model and solution approach, including the construction and solving of an IP, is given by [7] and [8]. While the former analyzes historical data given by the Turkish Coast Guard, the later concentrates on the development of a practical tool for the US Coast Guard. Both differ from our work in that their aim is to minimize the deviation from given values of budget and operating hours instead of minimizing individual response times. [7] is further expanded by [9] in which one of the authors explores several ways of improving the IP in terms of realism. Besides introducing a more diverse arsenal of rescue crafts it also considers how to implement and react to uncertainty in terms of incidents. Another IP-based approach is provided in [10]. Here, the authors use a two-stage approach to solve the IP, since the original formulation does not perform well computationally. For small instances, enumeration may also be possible, as showcased in [11].

Recent research by [12] focuses on the pacific ocean area the US Coast Guard is responsible for. While it shares many similarities to our work, it differs in the modeling of incidents. While we consider the incidents as being few enough that it can be assumed a needed vessel is at its harbour when the distress call comes in, [12] assigns every incident a certain amount of hours needed during which the responding vessel can not move to the next incident. Their work also includes the possibility of relocating vessels for a certain price. Finally, there is some overlap with [13], who only assign a number of homogeneous boats to sections, but do so addressing uncertainties through robust optimization.

The field of research regarding maritime search and rescue also has many works with a similar motivation but a different approach in terms of model and aim. Other related work primarily focuses on on the possible causes of incidents, and on how to compare and combine their severity [14]. [15] also deals with maritime search and rescue but in terms of searching a given area of a single incident.

An overview of the different sources and their properties is given in table Table 1.

As the first column shows, almost all sources have given stations and the *zones* column signals that nearly all of them are working with zones to describe and solve the optimization problem. The *vessel types* column indicates if a source considered vessels with different characteristics like we do or if the focus of allocation is on another aspect. The last two columns reveal that solving the problem is mostly done through a IP-solver rather than by using a specific algorithm.

For a broader overview over the topic of Search-and-Rescue (SAR) operations, we refer to the state of the art paper by [18]. The authors note that in general, the subject of this work, the allocation of assets (vessels) to stations (harbors) is one of multiple closely related fields, i.e., location modelling of SAR stations, allocation modelling of SAR assets, risk assessment modelling of SAR areas, and search theory and SAR planning modelling. For, a general discussion of SAR and its connection to other medical facility locations problems, including stochastic variations, we refer to [17].

## 3. Model

Next we formulate our model for the RCAP. Here, consideration of the tides is the most notable difference from the models of the previously listed sources.

source (comment)	given stations	vessel types	zones	IP	algorithm
Afshartous et al. $(2009)$ [5]	$\sim$	n	у	у	n
Conversion of incident data into i	incident p	robabili	ties		
Ai et al. $(2015)$ [16]	У	$\sim$	У	$\sim$	У
Comparison of heuristics for solu	tion findin	ıg			
Azofra et al. $(2007)$ [4]	У	n	У	$\sim$	n
Basic model for assigning a single	e vessel				
Chen et al. $(2021)$ [10]	у	У	у	у	У
Separation into tactical and oper-	ational ph	ase			
Jin et al. $(2021)$ [6]	n	У	у	n	У
Minimisation of construction and	maintena	nce cos	t		
Jung & Yoo (2019) [11]	$\sim$	n	У	n	У
Consideration of islands and coast	tline in di	stance	calculat	ion	
Feldens & Chen (2020) [15]	у	n	У	у	n
Maximisation of covered area in s	search and	l rescue	operat	ion	
Hoernberger et al. $(2020)$ [12]	у	$\sim$	У	у	n
Inclusion of relocation costs in re	gards to c	urrent a	allocatio	on	
Karatas $(2021)$ [9]	у	у	У	у	n
Considers tradeoff between respon	nse time, <sup>.</sup>	working	hours	and	budget
Ma et al. $(2024)$ [13]	$\sim$	n	$\sim$	у	n
Robust optimization					
Pelot et al. $(2015)$ [17]	у	у	У	у	n
Multiple modelling approaches					
Razi & Karatas (2016) [7]	у	у	у	у	n
Inclusion of different incident typ	es				
Wagner & Radovilsky (2012) [8]	у	у	n	у	n
Development of model for practic	al use				
Zhou et al. $(2022)$ [14]	у	n	У	n	n
Search and rescue from a game the	neoretical	perspec	tive		

Table 1: Literature on rescue vessel placement. The entries indicates [y]es or [n]o, with  $[\sim]$  denoting special cases.

# 3.1. Parameters

First we define the parameters needed for a single instance. For each instance, this includes information on the available vessels, stations and zones.

Regarding the available vessels, a defining trait is the total number of

different types of vessels  $n \in \mathbb{N}$ , the speed of each type of vessel  $v_1, \ldots, v_n \in \mathbb{N}$ , the draught of each vessel  $\delta_1, \ldots, \delta_n \in \mathbb{R}^+$  as well as the amount of available vessels for each type  $a_1, \ldots, a_n \in \mathbb{N}$ . In terms of stations, we need to know their total number  $m \in \mathbb{N}$  and, to represent the relationship between vessel types and stations, a set  $C \subseteq \underline{n} \times \underline{m}$ ,<sup>1</sup> where  $(i, j) \in C$  means that a vessel of type *i* can be positioned at station *j*.

Due to the tides the water level at each of the stations changes regularly which leads to vessels with a too high draught being unable to leave. To model this, we consider data of the tides in a period  $\mathcal{T}$ . We then consider each point of time  $t \in \mathcal{T}$  and collect all usable combinations of vessels and stations  $e \subseteq \underline{m} \times \underline{n}$  at that point of time t. We define a uncertainty set  $\mathcal{U} \subseteq \mathcal{P}(\underline{m} \times \underline{n})$  that contains all usable configurations e.

The incidents the vessels respond to are grouped into  $f \in \mathbb{N}$  types with severities  $w_1, \ldots, w_f \in \mathbb{R}$ . Since some incident types may require specific features of a vessel, such as enough weight and power to tow a heavy vessel, the set  $B \subseteq \underline{n} \times f$  represents compatibility between vessel and incident types.

The territory to be covered is divided into  $z \in \mathbb{N}$  zones, which have certain distances to the stations represented by  $d_{jr}$  for the distance between station j and zone r. Because not every vessel can reach every zone from every station (e.g., due to tank size or offshore unsuitability), we have a set  $S \subseteq \underline{n} \times \underline{m} \times \underline{z}$  representing the compatible vessel-station-zone-combinations.

### 3.2. Feasible Solutions

A feasible solution consists of two parts. The first one represents the allocation of the vessel types to the stations. Let G be a graph whose nodes represent all vessel types and all stations and whose edges are given by the set of compatible combinations C. A solution consists of a (not necessarily optimal) bipartite b-Matching M with  $b(v) = a_i$  if  $v \in V(G)$  represents vessel type i and b(v) = 1 if it represents a station. A vessel type i is assigned to a station j if the edge between their nodes is part of M.

The second part of a feasible solution ensures that every incident can be responded to. It is a mapping  $u : \underline{f} \times \underline{z} \times \mathcal{U} \to \underline{m}$  that assigns every combination of incident type k, zone r and water state e a responding station j and, combined with M, a responding vessel type i. This mapping has to adhere to the limitations outlined above: The vessel type must be able to

 $<sup>{}^{1}\</sup>underline{n} \coloneqq \{1, \ldots, n\} \text{ for } n \in \mathbb{N}$ 

help with the incident type meaning  $(i, k) \in B$ , it must be able to traverse the distance between harbour and zone meaning  $(i, j, r) \in S$  and the station must have a high enough water level to be operational for the vessel so  $(j, i) \in e$ .

#### 3.3. Objective Function

The aim of our model is to minimize the average weighted response time to incidents at sea. For every combination (k, r, e) of incident type, zone and water state and their responding station j = u(k, r, e), there is a distance  $d_{jr}$ . Let *i* be the vessel type of the node matched to the node of *j* in *M*. Dividing the distance by the speed  $v_i$ , a response time can be calculated. The average weighted response time of a solution is defined as the sum of all response times, each multiplied by the severity  $w_k$  of the incident type.

$$\min_{\substack{(k,r,e)\in f\times z\times \mathcal{U}\\j=u(k,r,e)}} \mathbb{E}\left(\frac{d_{jr}}{v_i}w_k\right).$$
(1)

We assume that for every zone r and incident type k there is a frequency  $q_{kr} \in [0, 1]$  of an incident type occurring in the given zone. To track how often each usable configuration e appears in the whole time period  $\mathcal{T}$ , we set  $\tilde{p}_e \in [0, 1]$  to the percentage of time it occurs. Note that the equation

$$\sum_{e \in \mathcal{U}} \tilde{p}_e = 1$$

is true, since at every point of time  $x \in \mathcal{T}$  exactly one configuration e occurs. Thus, we can reformulate the objective as

$$\min \sum_{\substack{(k,r,e)\in f\times z\times\mathcal{U}\\j=u(k,r,e)}} \frac{d_{jr}}{v_i} w_k q_{kr} \tilde{p}_e.$$
(2)

To summarize, an overview of all parameters and variables is given in Table 2.

## 4. Complexity

In this section, we examine the complexity of the RCAP. We show that the feasibility problem corresponding to RCAP is  $\mathcal{NP}$ -hard by reduction from Exact Cover by 3-Sets Problem (X3CP). Based on this, we argue that the RCAP is  $\mathcal{NPO}$ -complete.

Variable	Element of	Usage
$a_i$	Z	amount of vessels of type <i>i</i> available
В	$\mathcal{P}(\underline{n}  imes f)$	$(i,k) \in B$ if vessel type i has the equipment required for incident type k
C	$\mathcal{P}(\underline{n}  imes \overline{\underline{m}})$	$(i, j) \in C$ if vessel type i can be placed at station j
$d_{jr}$	+出	distance between station $j$ and zone $r$
e ,	$\mathcal{P}(\underline{n}  imes \overline{m})$	state of tides in which exactly the vessel-station combinations $(i, j) \in e$ are available
$\mathcal{N}$	$\mathcal{P}(\mathcal{P}(\underline{n}  imes \underline{m}))$	uncertainty set of tide states with non-zero probability
f	N	amount of incident types
i	$\overline{u}$	index referring to a certain vessel type
j	$\overline{m}$	index referring to a certain station
k	f	index referring to a certain incident type
m	N	amount of stations
M		<i>b</i> -matching representing the vessel-station-allocation
u	N	amount of vessel types
$ ilde{p}_e$	[0,1]	probability of tidal state $e$ occurring
$q_{kr}$	[0,1]	frequency of incident type $k$ occuring in zone $r$
r	2	index referring to a certain zone
S	$\mathcal{P}(\underline{n} \times \underline{m} \times \underline{z})$	$(i, j, r) \in S$ if vessel type i can travel from station j to zone r
n		the vessel of station $u(k, r, e)$ responds to incident-zone-tide combination $(k, r, e)$
$v_i$	民+	speed of vessel type $i$
$w_k$	民+	severity of incident type $k$
$\mathcal{X}$	$\mathcal{P}(\underline{n}  imes \overline{m})$	set of all possible vessel-station combinations
S	$\mathcal{P}(\underline{n} \times \underline{m} \times \underline{f} \times \underline{z} \times \underline{\mathcal{U}})$	set of all possible vessel-station-incident-zone-tide combinations
\$	Z	amount of zones
$\delta_i$	民+	draught of vessel type $i$
	Table 9.	$Our minimum methods and on in - 11 models for m \in \mathbb{N}$

Table 2: Overview variables where  $\underline{x} \coloneqq \{1, \ldots, x\}$  for  $x \in \mathbb{N}$ 

**Definition 1.** Let A be an instance of the RCAP. We define the Feasibility Rescue Craft Allocation Problem (f-RCAP) as the problem of finding a feasible solution for A, or proving that no such solution exists.

Note that the f-RCAP is a decision problem, whereas RCAP is an optimization problem. We do all proofs for the decision problem and then extend them to the optimization problem.

**Lemma 2.** The f-RCAP is in  $\mathcal{NP}$ .

*Proof.* A solution must consist of a function  $M : \underline{m} \to \underline{n}$  assigning every station in  $\underline{m}$  a vessel in  $\underline{n}$  as well as a function  $u : \underline{f} \times \underline{z} \times \mathcal{U} \to \underline{m}$  assigning every water state e, zone in  $\underline{z}$  and incident type in  $\underline{f}$  a responding station in  $\underline{m}$ .

Given these, a in a feasible solution harbours only house compatible vessels, meaning  $(j, M(j)) \in C$  for all  $j \in \underline{m}$ , which can be done in  $\mathcal{O}(m)$ . Furthermore we need to:

- Verify that the vessel of the responding station is operable during the given water state, i.e., the harbour vessel combination must be in *e*.
- Ensure, that the vessel is equipped to deal with the given incident, meaning  $(M(u(k, r, e)), k) \in B$  must be true for all  $k \in f$ ,  $r \in \underline{z}$ ,  $e \in \mathcal{U}$ .
- Check that the given zone in z is reachable from the specified station by the responding vessel, meaning  $(M(u(k, r, e)), u(k, r, e), r) \in S$  must be true for all  $k \in f, r \in \underline{z}, e \in \mathcal{U}$ .

Since each of these categories requires either  $\mathcal{O}(m)$  or  $\mathcal{O}(fz|\mathcal{U}|)$  checks with a runtime of  $\mathcal{O}(1)$  each, in total we have a polynomial runtime of  $\mathcal{O}(m + fz|\mathcal{U}|)$ .

**Lemma 3.** f-RCAP is  $\mathcal{NP}$ -hard, even for only two vessel types, disregarded differing vessel-ranges, vessel-station incompatibilities, incident types and water states.

*Proof.* We use the X3CP to prove the  $\mathcal{NP}$ -hardness of the f-RCAP. Each instance of the X3CP consists of a set X with  $q := \frac{|X|}{3} \in \mathbb{N}$  and a set  $D \subseteq \{x \subseteq X : |x| = 3\}$ . For this instance the decision problem is whether there exists a subset  $A \subseteq D$  such that |A| = q and  $\bigcup A = X$ . This problem is a known  $\mathcal{NP}$ -complete problem, see [19, 221].

Given an instance of the X3CP, we now construct an equivalent RCAP instance. To do so we create one zone per element of X, one station for each set in D, and two vessel types I and II. We only create a singular incident type of severity 1 and probability 1 in every zone. The distance from any station to any zone is set to 1 and the speed of all vessels is set to 1 as well. There are q vessels of type I and |D| - q of type II available. Each vessel is operable in every station at all times. All vessels can be assigned to any of the stations. Vessels of type II can not reach any zone from any of the harbours, vessels of type I positioned at the station corresponding to  $d \in D$ can reach all zones corresponding to one of the elements in d. Every vessel type is capable of assisting with the single incident type.

To show such an instance is equivalent to the original we will prove that a feasible solution to the RCAP-instance exists if and only if the X3CP instance is a yes-instance.

First, starting with a solution to the RCAP, let A be the set of all elements of D which correspond to stations that have a vessel of type I assigned to them. This is a solution to the X3CP as there are q ships of type I, so |A| = qand all 3q zones are covered, while each station can cover up to 3 zones with a vessel of type I and 0 zones with type II. Due to z = 3q this means that each station with a vessel of type I assigned covers exactly 3 zones, thereby all of the elements of X occur in exactly one set in A and  $\bigcup A = X$ .

Second, starting with a solution A to the instance of the X3CP, we assign vessels of type I to all stations corresponding to an Element in A and vessels of type II to the remaining stations. Then for each zone with corresponding element  $x \in X$  exactly one station with a vessel of type I is capable of responding to incidents of the singular type in that zone as  $x \in \bigcup A$ . This gives a feasible (and optimal) solution.

As the two instances are equivalent and the transformation is polynomial this proves that the f-RCAP is  $\mathcal{NP}$ -hard.

**Theorem 4.** f-RCAP is  $\mathcal{NP}$ -complete, even for only two vessel types, disregarded differing vessel-speeds, vessel-station incompatibilities, incident types and water states.

*Proof.* This follow immediately from Theorem 2 and Theorem 3.  $\Box$ 

**Corollary 5.** RCAP is NPO-complete, even for only two vessel types, disregarded differing vessel-speeds, vessel-station incompatibilities, incident types and water states.

*Proof.* This follow immediately from the  $\mathcal{NP}$ -completeness of f-RCAP.  $\Box$ 

Note that we could equally formulate Theorem 3 in terms of ranges, not inabilities to reach certain zones. Furthermore, note that the two different vessel types and their (in)ability to reach the incident zones were key to our reduction. This difference can alternatively be replaced by a difference in speed:

**Corollary 6.** RCAP is  $\mathcal{NPO}$ -complete, even for only two vessel types, disregarded differing vessel-ranges, vessel-station incompatibilities, incident types and water states.

*Proof.* We assign vessel type I a speed of  $v_{I} = 1$  and vessel type II a speed of  $v_{II} = 0.5$  (and set all distances to  $d_{jr} = 1$ ). The goal equivalent to finding a solution for the X3CP-instance is to find a solution for the constructed RCAP-instance with a total response time of at most 3q. Since every one of the 3q zones contributes either 1 or 2 to the total response time depending on the vessel responding, a total of 3q is equivalent to using only the q vessels of type I to respond to the incidents.

In conclusion, there is no singular aspect of the RCAP responsible for its complexity because any feature used in the transformation by itself can be replaced by a combination of the other parameters.

## 5. Integer Program for RCAP

The problem of rescue craft-allocation can be modeled as a (binary) IP as seen below. In this context, the variable  $x_{ij} \in \{0, 1\}$  represents the decision to assign a ship of type  $i \in \underline{n}$  to station  $j \in \underline{m}$  while the variable  $y_{ijkre}$ represents the decision to let a ship of type i positioned at station j attend to incidents of type  $k \in \underline{f}$  occurring in zone  $r \in \underline{z}$  during the water state  $e \in \mathcal{U}$ . In order to avoid creating unnecessary variables due to the constraints given by  $C, B, \mathcal{U}$  and S we define the sets

$$\mathcal{X} \coloneqq \{(i,j) \in \underline{n} \times \underline{m} : (i,j) \in C\} \text{ and}$$
(3)

$$\mathcal{Y} \coloneqq \{ (i, j, k, r, e) \in \underline{n} \times \underline{m} \times \underline{f} \times \underline{z} \times \mathcal{U} :$$
(4)

$$(i,j) \in \mathcal{X}, (i,k) \in B, (j,i) \in e, (i,j,r) \in S\}$$

$$\bar{\mathcal{Y}} \leftarrow \{(k,m,q) : (i,j,k,m,q) \in \mathcal{Y}\}$$
(5)

$$\mathcal{V}_{ij} \coloneqq \{(k, r, e) : (i, j, k, r, e) \in \mathcal{Y}\}.$$
(5)

Using these we can describe our problem as a IP as follows

min  $\sum_{(i,j,k,r) \in \mathcal{V}} \frac{d_{jr}}{v_i} q_{kr} \tilde{p}_e w_k y_{ijkre}$ 

s.

t. 
$$\sum_{\substack{i,j:\\(i,j,k,r,e)\in\mathcal{Y}}}^{(i,j,k,r,e)\in\mathcal{Y}} y_{ijkre} \ge 1 \qquad \forall k \in \underline{f}, r \in \underline{z}, e \in \mathcal{U}$$
(6a)

$$\sum_{(k,r,e)\in\bar{\mathcal{Y}}_{ij}} y_{ijkre} \le |\bar{\mathcal{Y}}_{ij}| x_{ij} \qquad \forall (i,j) \in \mathcal{X}$$
(6b)

$$\sum_{j:} x_{ij} \leq a_i \qquad \forall i \in \underline{n}$$
(6c)

$$\sum_{\substack{i:\\(i,j)\in\mathcal{X}}}^{i:i,j)\in\mathcal{X}} x_{ij} \le 1 \qquad \forall j \in \underline{m}$$
(6d)

$$\begin{aligned} x_{ij} \in \{0,1\} & \forall (i,j) \in \mathcal{X} \\ y_{ijkre} \in \{0,1\} & \forall (i,j,k,r,e) \in \mathcal{Y} \end{aligned}$$
 (6e) (6f)

Our objective function (which is similar to Eq. (2)) is the sum of the vesselstation-zone-state-incident-assignments, each weighted by the incident-frequency  $q_{kr}$ , the probability of the water state  $\tilde{p}_e$ , the incident-severity  $w_k$  and most importantly the traveling time  $\frac{d_{jr}}{v_i}$ . Constraint 6a is used to ensure every zone-time-incident-combination is attended to and Constraint 6b ensures that a vessel is stationed at the station it is sent out from. Constraint 6c limits the amount of vessels assigned to the number of vessels available for every vessel type. Constraint 6d ensures that every station has at most one vessel assigned to it.

Initial computational testing showed that the explicit, stochastic version of the IP provided above performs badly in practice and starkly limits the possible resolution of zones. Thus, we also provide two subject-specific simplifications, which we evaluate in Section 6.

## 5.1. Corrected water levels for Stations and Vessels

As the Baltic and the Northern Sea are continuous bodies of water within a limited geographical area, for both seas the tides at different locations are strongly correlated. We validated this for the tide data used in this work, as shown in Appendix A. The data sourcing is covered in more detail in Section 6. Based on this, we can make the simplifying assumption that during the time frame a specific station-vessel combination is operable, all combinations that are overall more frequently available are also operable.

This means we sort the station-vessel combinations by relative availability and instead of considering all possible combinations of operable stations (the set  $\mathcal{U}$ ) we only focus on situations where the most frequently available stationvessel combinations are operable. In practical terms, we calculate

$$\tilde{p}_{(j,i)} \coloneqq \sum_{e \in \mathcal{U}} \mathbf{1}_e((j,i)) \tilde{p}_e$$

as the relative availability of the station-vessel combination  $(j, i) \in \underline{m} \times \underline{n}$ where **1** is the indicator function. We define the set of availabilities as

$$P = \{\tilde{p}_{(j,i)} : (j,i) \in \underline{m} \times \underline{n}\} \cup \{0,1\}$$

and use the intervals

$$\bar{P} = \{ [p_1, p_2] \in P^2 : p_1 < p_2 \land \nexists p_3 : (p_1 < p_3 < p_2) \}$$

to replace E. This means that in the interval  $[p_1, p_2]$  we assume that all station-vessel combinations with a probability above  $p_1$  are available. Due to  $|E| \in \mathcal{O}(2^{mn})$  and  $|\bar{P}| \in \mathcal{O}(|P|) = \mathcal{O}(mn)$ , this simplification can significantly decrease the input size of an instance. The inaccuracy induced by this simplification is based on the difference in water levels across stations at the same point of time which is relatively small.

To adjust the IP from Section 5 it is mainly necessary to adjust Eq. (4) to

$$\mathcal{Y} \coloneqq \{ (i, j, k, r, t) \in \underline{n} \times \underline{m} \times \underline{f} \times \underline{z} \times \overline{P} :$$

$$(i, j) \in \mathcal{X}, (i, k) \in B, \tilde{p}_{(j,i)} \ge \min(t), (i, j, r) \in S \}$$

$$(7)$$

and all occurrences of  ${\mathcal U}$  accordingly. Additionally the target function must be changed to

$$\min \sum_{(i,j,k,r,t)\in\mathcal{Y}} \frac{d_{jr}}{v_i} q_{kr}(\max(t) - \min(t)) w_k y_{ijkrt},$$

which is still a linear function since  $\max(t)$  and  $\min(t)$  are constants.

#### 5.2. Corrected water levels for Stations

The simplification above can be further expanded on by averaging the water level of a station and deleting the dependence of the vessel stationed there. Given the  $\tilde{p}_{(j,i)}$  of the previous section, for a fixed station j we calculate

$$\tilde{p}_j \coloneqq \frac{\sum_{i \in \underline{n}} \tilde{p}_{(j,i)} a_i}{\sum_{i \in \underline{n}} a_i}$$

as relative availability by scaling the relative availability in combination with every vessel type by the vessel type amount. These further simplified water levels  $\tilde{p}_j$  can be used to replace the inequality  $\tilde{p}_{(j,i)} \geq \min(t)$  in Eq. (7) with  $\tilde{p}_j \geq \min(t)$ . This simplification further reduces the size of P to  $\mathcal{O}(m)$  instead of  $\mathcal{O}(nm)$  by averaging the draught values of all vessel types. The IP can be adjusted similarly to Section 5.1 while changing the corresponding indices from (j, i) to j.

## 6. Computational Study

We tested the IP variations on several instances of the problem. In the following, we give an overview of instance generation, the data used, assumptions made about the data, and the computational setup. We then explain how solutions were validated. The code and data are publicly available through GitHub [20].

#### 6.1. Available data

An instance consists of information about the vessel types, the stations, the incidents, the tide levels, and the relations thereof.

#### 6.1.1. Data on vessel types, stations and incidence types

The information about the vessel types and stations is based on [21], where the DGzRS lists the vessels and stations currently used. At the time of writing there are 11 types of vessels and 55 rescue stations. Every vessel type listed has a specifications sheet detailing information such as the speed of the vessel in knots, its reach depending on its speed in nautical miles, its draught in metres and information about its equipment such as material for firefighting or towing ships of several sizes. As the actual reach is dependent on the speed, which our model does not take into account, we always use the maximum given reach when deciding whether a vessel is capable of reaching a zone from a certain station. Regarding the stations, we extracted their coordinates. The positions of the stations are shown in Fig. 1. The vessel-station-compatibilities were randomly generated by giving each combination the probability p = 0.9 of being allowed. While the real world data gives



Figure 1: The red triangles show the positions of the 55 DGzRS-stations in the Northern and Baltic Sea.

indicators such as vessel length and current crew regarding this compatibility, it is insufficient to create clear rules of which combinations are appropriate.

Using the equipment list of the vessel types we manually define five incident types, requiring firefighting equipment, pumping equipment, a secondary craft, a board hospital, or requiring first aid (which every vessel offers). Additionally we create several incident types requiring towing vessels of various sizes. Using the equipment lists mentioned above we decide which vessels are able to respond to them. At instance generation, the severity of every incident type is set to a random value in [0, 1]. The frequency of an incident type occurring in a given zone is also randomly chosen in a two-step process: First if the incident type has a non-zero chance of occurring (with a value of p = 0.4 for positive) and if it does, a random value in [0, 1] for the actual frequency.

#### 6.1.2. Geographical data

In our study, we focus on the German territorial waters as detailed in [1]. In our implementation we work with the data from [22] using QGIS (see [23]) and its integrated Python-interface PyQGIS. We use their 100 meter grid to filter for those map squares which are completely covered by water and then dissolving this grid by calculating the connected components. The two biggest connected components represent the North and Baltic Sea quite closely because rivers and islands are excluded due to the 100 meter grid.

One main flaw however is that the *Tiefwasserreede*, a German exclave as detailed in [1], also is excluded.

## 6.1.3. Generation of zones

In order to generate zones we place 1000 random points in the polygon using a PyQGIS script. For the distance calculation between these zones and stations we use the direct distances between two points on the surface of the earth. This means we disregard possible obstacles like islands and restricted areas and also disregard possible currents and differences between tidal levels. To calculate the distances on the surface of the earth we used the haversine formula (implementation from the python haversine package<sup>2</sup>) with an earth radius of 6371 kilometers. These distances combined with the range of the vessel types (divided by two to account for the way back) decide if the vessel can travel between the zones and the stations. In order to make these instances solvable, similarly to [12], we then apply k-means clustering on the Geo locations. Figure 2 shows an example of the generated zones (500 meter grid instead 100 meters for better visualization).



Figure 2: Incident generation across North and Baltic Sea. Yellow dots represent zones generated (amount: 1000). Red dots represent clusters of zones (amount: 10).

When location points are combined to one point x we use the mean value of the incident rates of the old points for x. A side effect is smoothing the location values. Previously, a location point close to multiple incident locations would be considered completely harmless since no incidents happened exactly there. After clustering, these incidents indicate that this adjacent point should also be considered dangerous. For the implementation of k-

<sup>&</sup>lt;sup>2</sup>https://github.com/mapado/haversine

means clustering, a deterministic KMeans-method provided by the sklearnlibrary was used, see [24].

## 6.1.4. Data on Tide levels

For determining adequate tide levels, we consult [25] where the measurements of water gauges across both North and Baltic Sea are published as well as their position. These can be seen in Fig. 3.



Figure 3: Locations of the gauges used to determine the water levels

Due to the fact most station have no water level gauge at their exact location, we approximate their water level using the three closest gauges, weighted by their distance to the station. This data is recorded every minute and stored for one month. For our tests we use the data between Monday 20<sup>th</sup> November, 2023 and Wednesday 20<sup>th</sup> December, 2023, although older data can be requested from the Bundesanstalt für Gewässerkunde and estimates for the future are done by the Bundesamt für Seeschifffahrt und Hydrographie. We gain depth data for the stations from [26]. In cases where no measurement for the exact location is given, a closest point is used. In practical application a safety margin might be necessary, which we do not consider for now. In total, we arrive at around 8700 different tidal states.

By dividing the data into the North Sea and and the Baltic Sea we receive two additional smaller data sets that could be used for further comparisons. As the DGzRS however does not need to plan for them independently but simultaneously for both we do not include this in our computational study.

## 6.2. Setup for the study

The code was written in Python (Version 3.11.2) with Gurobi (Version 10.0.0, [27]) and was executed on the High Performance Cluster of the RWTH

Aachen<sup>3</sup>, using Intel Xeon Platinum 8160 Processors (2.1 GHz).

The three different approaches are named *many-zones* (Section 5.2), *better-tidal* (Section 5.1) and *best-tidal* (Section 5). For comparability the instances of all three approaches run on a single core CPU. Since runtime and RAM limitation is needed for the usage of the High Performance Cluster, we cap both. To ensure a solution by Gurobi, we set the *TimeLimit* property of Gurobi to 6 hours and limit the total time for the jobs on the Cluster to 9 hours.

All instances are initialized with the same 1000 zones. Because this amount is too high for all approaches, we use the k-means clustering algorithm to shrink them down to a desired number  $n_z \in \{1, \ldots, 1000\}$ . As *better-tidal* is more difficult to solve than *many-zones*, the approach *manyzones* uses  $n_z \in \{10, 50, 100\}$  zones for problem solving while *better-tidal* uses  $n_z \in \{10, 20, 30\}$  zones. Both approaches have access to 32GB RAM. Because *best-tidal* is very hard to solve, we only use the values  $n_z \in \{1, 2, 5\}$ for it with access to 64GM RAM. The fact that the job with  $n_z = 5$  did run out of memory led us to the decision to discard this job for to practical concerns. To compare the different approaches we calculate all solutions on the objective function of *best-tidal* on all 1000 zones. For evaluation we run each configuration with 10 different seeds for the random parameters. This means in total we have  $10 \cdot 3$  instances for every approach, which results in 90 jobs overall.

# 6.3. Prelininary computational results

First, the build times of the models, as can be seen in Fig. 4, already limit the usability of *best-tidal*. This, combined with the huge memory requirement of *best-tidal* as can be seen in Fig. 5, validates that running *best-tidal* without zone clustering is not viable. Therefore it is necessary to compare the solution quality of different heuristics and different amounts of zone clusters, as for example 100 zone clusters in *many-zones* result in more memory efficiency and a lower run time than 2 clusters in *best-tidal*. To do so, we extract the vessel-station assignment M of every solution. We then validate the second part of the solution (u) by checking for all combinations of each of the original 1000 zones, each incident type and each tidal state (according to our best

<sup>&</sup>lt;sup>3</sup>https://web.archive.org/web/20240107173048/https:// help.itc.rwth-aachen.de/service/rhr4fjjutttf/article/ fbd107191cf14c4b8307f44f545cf68a/



Figure 4: Time required to build the Gurobi Models and cluster the zones.

available tidal data) which of the stationed compatible vessels can respond the fastest. In this process we also confirm that all of the produced solutions for the different instances are feasible.

# 7. Discussion

The resulting objective values can be seen in Fig. 6. It is important to note that not every instance has the same optimal solution value.

Looking at the values it is clear that in our instances we gain better results with a higher amount of zone clusters in exchange for a reduction in tidal states. This is an be explained by the correlation between the tidal levels at the different stations, as noted before. Additionally we see that the difference between *better-tidal* and *many-zones* is rather small. This is most likely due to the fact that the vessels have quite similar draught, the vessel with the lowest value has 0.5 meters while the one with the highest has 2.7 meters. Furthermore, *many-zones* is more memory efficient and managed, unlike *better-tidal*, to sometimes find the optimal solution to the simplified problem within the time limit and therefore exited faster. We can also see that clustering to a small amount of zones does not seem to have a big



Figure 5: Memory usage of the complete instances with 1000 zones and the complete tidal information. The x-axis is log scaled for better readability.

influence on *many-zones* and *better-tidal*.

Note that currently the vessel-station-compatibility is randomized. This has to be replaced with data of the DGzRS detailing if a vessel could be placed at a station, taking the vessel size and crew into account. For example a vessel can not be placed at a station if it is too large or if the locally available staff size is too low. For non-randomized incident rates, it might be worthwhile to overhaul the concept of zones. It is more appropriate to divide the region into equally sized zones. Currently this can not be done because increasing the base amount of zones leads to convergence against the same incident rates with k-means clustering. Real world incident data would allow for equally sized zones without such statistical issues. However the exact amount of zones would be less controllable, since the input parameter for the zone creation would be zone size instead of zone amount.

At the moment tide data is used to determine availability of stations. Of course zones are also affected by the tides. It might be worthwhile to also give the zones a tide property and expand route calculation to note temporarily inaccessible zones. Moreover tides impacts the travel time. Considering all these aspects would lead to an even larger and more complex model.



Figure 6: Objective Value in the complete instances with 1000 zones and the complete tidal information.

To improve the accuracy of the results, better tide data could be used. A possibility is to enlarge the time horizon of tide data to one year and average it. Another possibility is to use forecast data to make the results more reliable for future planning.

# 8. Conclusion

In this work, we built a mathematical model for the Rescue Craft Allocation Problem (RCAP). While in general, RCAP is  $\mathcal{NP}$ -hard and formulating it as a IP leads to large formulations, there are approaches to effectively reduce the problem size. We have shown that clustering of incidents as well as simplification of the possible tide states lead to significant run time reductions. The degree of simplification regarding the tide states can be varied.

In order to compare these approaches we set up a computational study in which we tested them under restricted resources in regards to memory and runtime. To do so we used real world data of the Deutsche Gesellschaft zur Rettung Schiffbrüchiger (German Maritime Search and Rescue Service) (DGzRS) and other sources. Some of the data such as incidents and vesselstation compatibility was generated randomly due to lacking data. Furthermore, this lack of data is also the reason for not comparing our results to the solution currently used, as our results might be infeasible in practice and the real solution in turn infeasible for our instances.

Our computational study establishes the validity of our concept of simplified tide representation and clustering of the incident zones. As shown in Fig. 6 there is no significant difference in quality between *better-tidal* and *many-zones*. Beyond that *best-tidal* returns worse results. Since, in the context of our computational study, using more zones didi not lead to better results, using a k-means clustering algorithm (Section 6.1.3) has shown to be a good approach. Moreover we obtained feasible solutions, which indicates a practical ability of our model. It might therefore make sense to test apply the model to real world data of the DGzRS to attempt improving their current assignment.

# 8.1. Further research

The model presented in this work can be expanded on in multiple ways. First of all, the estimation of incident risk can be further refined. Part of this would be to introduce an uncertainty factor so that calculated solutions are robust to changes in incident data.

Second, our assumption is that every incident is isolated, meaning a vessel can respond to an infinite number of incidents. While the number of incidents suggests a daily average of less than six incidents across the entire region making it unlikely that a vessel is required at two location simultaneously, it might be worthwhile to balance the workload across the vessels available.

Third, in our model the assumption is that the amount of vessels is fixed. If this number is reduced, it might be interesting to analyze which vessel should be removed and what the increase in response times would be. Conversely, it is not trivial which improvement an additional vessel would make and where to place it.

Fourth, we only consider the haversine distance between harbors and zones. However, in the real-world factors, like fairway, depth of water, restricted areas and even the location of islands have to be considered when computing a route. Implementing this would serve to make the modelling more valid to practitioners. Furthermore, as suggested by [28], wind and wave patterns also influence rescue speed, which would lend itself to stochastic optimization. Finally it would be interesting to see if there are yearly patterns in the incident data and how beneficial a seasonal reallocation of the rescue vessels would be.

Appendix A. Tide Correlation Data

_																														
_	9610	010 9610015	9610020 96	10025 961	0035 96100	40 9610045	9610050	9610066	9610070	9610075 9	610080 9	630007	9630008 96	40015 96500	4 9650030	9650040	9650043	9650070	9650073	9650080 96	570046 9	670050 1	9670055	9670063	9670065	9670067	9690077	9690078	9690085	9690063
961	0010 1	1.00 1.00	1.00	0.24	0.96 0	.82 0.95	0.99	0.99	0.97	0.96	0.95	0.94	0.93	0.91 0.	13 0.52	0.90	0.92	0.91	0.89	0.83	0.84	0.88	0.80	0.89	0.83	0.86	0.85	0.80	0.85	0.79
961	0015 1	1.00 1.00	1.00	0.24	0.96 0	.81 1.00	0.99	0.99	0.97	0.97	0.96	0.95	0.94	0.92 0.	12 0.51	0.90	0.93	0.92	0.90	0.83	0.85	0.88	0.81	0.90	0.84	0.87	0.86	0.82	0.86	0.80
961	0020 1	1.00 1.00	0.24	0.24	0.96 0	10 0.25	0.25	0.99	0.98	0.97	0.96	0.95	0.94	0.93 0.	1 0.51	0.91	0.93	0.92	0.90	0.07	0.85	0.89	0.81	0.90	0.84	0.87	0.86	0.82	0.86	0.81
961	0035 0	0.96 0.96	0.96	0.18	1.00 0	.94 0.96	0.96	0.95	0.92	0.93	0.93	0.91	0.90	0.89 0.	55 0.64	0.90	0.93	0.91	0.88	0.89	0.93	0.92	0.87	0.88	0.82	0.85	0.84	0.78	0.87	0.77
961	0040 0	0.82 0.81	0.81	0.10	0.94 1	.00 0.83	0.81	0.81	0.76	0.79	0.80	0.76	0.75	0.74 0.	37 0.72	0.80	0.84	0.82	0.78	0.87	0.92	0.87	0.85	0.79	0.71	0.74	0.75	0.67	0.81	0.65
961	0045 0	199 1.00	1.00	0.25	0.96 0	.81 1.00 81 1.00	1.00	1.00	0.98	0.98	0.97	0.95	0.95	0.93 0.	12 0.52	0.91	0.93	0.93	0.91	0.84	0.85	0.89	0.82	0.91	0.86	0.88	0.87	0.84	0.87	0.82
961	0066 0	1.99 0.99	0.99	0.25	0.95 0	.81 1.00	1.00	1.00	0.99	0.98	0.97	0.96	0.96	0.94 0.	1 0.52	0.92	0.93	0.93	0.92	0.84	0.84	0.89	0.82	0.91	0.87	0.89	0.88	0.85	0.88	0.84
961	0070 0	0.97 0.97	0.98	0.26	0.92 0	.76 0.96	0.99	0.99	1.00	0.99	0.97	0.98	0.98	0.97 0.	36 0.50	0.93	0.93	0.93	0.92	0.83	0.82	0.89	0.83	0.92	0.88	0.91	0.90	0.87	0.89	0.87
961	0015 0	0.95 0.96	0.97	0.25	0.93 0	.19 0.98	0.98	0.97	0.97	0.99	1.00	0.99	0.99	0.98 0.	1 0.54	0.94	0.95	0.95	0.94	0.86	0.85	0.91	0.85	0.95	0.92	0.93	0.95	0.91	0.91	0.50
963	0007 0	0.94 0.95	0.95	0.26	0.91 0	.76 0.96	0.97	0.96	0.98	0.99	0.99	1.00	1.00	0.99 0.	8 0.53	0.95	0.94	0.94	0.95	0.85	0.82	0.91	0.84	0.94	0.93	0.93	0.92	0.91	0.91	0.91
963	0008 0	0.93 0.94	0.94	0.26	0.90 0	.75 0.96	0.96	0.96	0.98	0.99	0.99	1.00	1.00	0.99 0.	37 0.53	0.95	0.93	0.94	0.94	0.85	0.81	0.90	0.84	0.94	0.92	0.93	0.92	0.91	0.91	0.91
965	0015 0	0.43 0.42	0.93	-0.18	0.55 0	.67 0.42	0.93	0.94	0.36	0.98	0.97	0.35	0.37	0.35 1.	0 0.92	0.96	0.94	0.93	0.95	0.64	0.61	0.55	0.60	0.44	0.39	0.93	0.44	0.36	0.52	0.33
965	0030 0	0.52 0.51	0.51	-0.14	0.64 0	.72 0.55	0.53	0.52	0.50	0.54	0.55	0.53	0.53	0.53 0.	2 1.00	0.64	0.63	0.62	0.61	0.80	0.74	0.71	0.79	0.61	0.57	0.61	0.64	0.56	0.72	0.55
965	0040 0	1.90 0.90	0.91	0.18	0.90 0	.80 0.91	0.92	0.92	0.93	0.96	0.94	0.95	0.95	0.96 0.	17 0.64	1.00	0.98	0.99	0.99	0.94	0.90	0.97	0.94	0.99	0.96	0.99	0.99	0.95	0.98	0.95
965	0070 0	0.91 0.92	0.92	0.18	0.91 0	.82 0.93	0.93	0.93	0.93	0.96	0.95	0.94	0.94	0.95 0.	17 0.62	0.99	0.99	1.00	0.99	0.93	0.91	0.97	0.92	0.99	0.95	0.98	0.98	0.94	0.97	0.93
965	0073 0	1.89 0.90	0.90	0.19	0.88 0	.78 0.91	0.92	0.92	0.92	0.95	0.94	0.95	0.94	0.96 0.	13 0.61	0.99	0.98	0.99	1.00	0.92	0.88	0.96	0.92	1.00	0.97	0.99	0.99	0.96	0.97	0.96
963	0080 0	1.83 0.83	0.83	0.07	0.89 0	.87 0.84 92 0.85	0.85	0.84	0.83	0.87	0.86	0.85	0.85	0.86 0.	54 0.80 51 0.74	0.94	0.94	0.93	0.92	0.96	0.96	0.97	0.99	0.93	0.88	0.92	0.93	0.87	0.98	0.86
967	0050 0	0.88 0.88	0.89	0.15	0.92 0	.87 0.85	0.90	0.89	0.89	0.93	0.91	0.91	0.90	0.91 0.	55 0.71	0.97	0.98	0.97	0.96	0.97	0.96	1.00	0.97	0.97	0.92	0.96	0.96	0.91	0.97	0.89
967	0055 0	0.80 0.81	0.81	0.11	0.87 0	.85 0.85	0.83	0.82	0.83	0.86	0.85	0.84	0.84	0.86 0.	50 0.79 M 0.61	0.94	0.93	0.92	0.92	0.99	0.95	0.97	1.00	0.92	0.88	0.92	0.93	0.88	0.97	0.87
967	1065 0	0.83 0.84	0.84	0.24	0.82 0	.71 0.86	0.87	0.87	0.88	0.92	0.91	0.93	0.92	0.94 0.	20 0.57	0.96	0.93	0.95	0.97	0.88	0.81	0.92	0.88	0.97	1.00	0.97	0.97	0.99	0.94	0.99
967	0067 0	0.86 0.87	0.87	0.19	0.85 0	.74 0.88	0.89	0.89	0.91	0.93	0.92	0.93	0.93	0.95 0.	12 0.61	0.99	0.97	0.98	0.99	0.92	0.86	0.96	0.92	0.99	0.97	1.00	0.99	0.97	0.98	0.97
969	0077 0	1.85 0.86	0.86	0.14	0.84 0	.75 0.87	0.88	0.88	0.90	0.93	0.91	0.92	0.92	0.94 0.	14 0.64 N 0.56	0.99	0.97	0.98	0.99	0.93	0.87	0.96	0.93	0.99	0.97	0.99	1.00	0.97	0.98	0.97
969	0085 0	1.85 0.86	0.86	0.14	0.87 0	.81 0.85	0.88	0.88	0.89	0.91	0.90	0.91	0.91	0.92 0.	12 0.72	0.98	0.97	0.97	0.97	0.98	0.92	0.97	0.97	0.97	0.94	0.98	0.98	0.94	1.00	0.94
969	0093 0	0.80 0.80	0.81	0.24	0.77 0	.65 0.85	0.84	0.84	0.87	0.90	0.89	0.91	0.91	0.93 0.	34 0.55	0.95	0.90	0.93	0.96	0.86	0.77	0.89	0.87	0.96	0.99	0.97	0.97	1.00	0.94	1.00
		9340020	934003	30 936	0010 9	390010	941001	0 95	10010	951006	0 95	10063	95100	66 9510	070 95	10075	951009	05 95	10132	953001	0 953	30020	9550	021 9	357001	0 957	0040	957003	50 95	370070
_		9340020	93400	30 936	0010 9	390010	941001	0 95	10010	951006	0 95	10063	95100	66 9510	070 95	10075	951009	95 95	10132	953001	0 953	30020	9550	021 9	957001	0 957	0040	95700	50 95	570070
9;	340020	9340020	93400	30 936 19	0010 9	0.94	941001	0 95	0.63	951006	i0 95:	10063 0.83	95100 0.	66 9510 74 (	070 95 .84	0.84	951009	05 95 59	0.43	953001 0.4	0 953	30020 0.23	9550	021 9	0.3	0 957 6	0.01	95700	50 95 24	-0.03
9; 9;	340020 340030	9340020 1.00 0.99	934003 0.9 1.0	30 936 )9 )0	0010 9 0.99 0.96	0.94 0.88	941001 0.9 0.8	0 95 12 15	10010 0.63 0.52	951006 0.3 0.2	i0 95: 14 19	10063 0.83 0.74	95100 0. 0.	66 9510 74 ( 66 (	070 95 .84 .75	0.84 0.75	951009 0.5 0.4	05 95 59 17	0.43 0.34	953001 0.4 0.3	0 953 3 1	0.23 0.10	9550	021 9 0.36 0.23	0.3 0.2	0 957 6 3	0.01 -0.11	957003 0.3 0.	50 95 24 12	-0.03 -0.14
9; 9; 9;	340020 340030 360010	9340020 1.00 0.99 0.99	934003 0.9 1.0 0.9	30 936 )9 )0 )6	0010 9 0.99 0.96 1.00	0.94 0.98 0.98	941001 0.9 0.8 0.9	0 95 12 15 16	10010 0.63 0.52 0.73	951006 0.3 0.2 0.3	i0 95: 14 19 18	0.83 0.74 0.90	95100 0.' 0.'	66 9510 74 ( 66 ( 80 (	070 95 .84 .75 .91	0.84 0.75 0.91	951009 0.5 0.4 0.6	05 95 59 17 59	0.43 0.34 0.50	953001 0.4 0.3 0.5	0 953 3 1 5	30020 0.23 0.10 0.36	9550	021 9 0.36 0.23 0.49	0.3 0.2 0.4	0 957 6 3 8	0.01 -0.11 0.14	957003 0.3 0.3	50 95 24 12 37	-0.03 -0.14 0.09
93 93 93 93	340020 340030 360010 390010	9340020 1.00 0.99 0.99 0.94	934003 0.5 0.5 0.5	30 936 19 10 16 38	0010 9 0.99 0.96 1.00 0.98	0.94 0.98 0.98 1.00	941001 0.9 0.8 0.9 1.0	0 95 12 15 16	10010 0.63 0.52 0.73 0.85	951006 0.3 0.2 0.3 0.4	i0 95 14 19 18 12	0.83 0.74 0.90 0.96	95100 0. 0. 0. 0.	66 9510 74 ( 66 ( 80 ( 87 (	070 95 .84 .75 .91 .97	0.84 0.75 0.91 0.97	951009 0.5 0.4 0.6 0.8	05 95 59 17 39 32	0.43 0.34 0.50 0.59	953001 0.4 0.3 0.5 0.7	0 953 3 5 70	30020 0.23 0.10 0.36 0.53	9550	021 9 0.36 0.23 0.49 0.64	0.3 0.2 0.4 0.6	0 957 6 3 8 4	0.01 -0.11 0.14 0.31	957003 0.: 0.: 0.:	50 95 24 12 37 53	-0.03 -0.14 0.09 0.25
9; 9; 9; 9; 9;	340020 340030 360010 390010 410010	9340020 1.00 0.99 0.99 0.94 0.92	934003 0.5 0.5 0.5 0.5 0.5	30 936 19 10 38 35	0.99 0.96 1.00 0.98 0.96	0.94 0.98 0.98 1.00 1.00	941001 0.9 0.8 0.9 1.0 1.0	0 95 12 15 16 10	10010 0.63 0.52 0.73 0.85 0.88	951006 0.3 0.2 0.3 0.4 0.4	i0 95 14 19 18 12 13	10063 0.83 0.74 0.90 0.96 0.98	95100 0.1 0.2 0.3 0.3 0.3	66 9510 74 ( 66 ( 80 ( 87 ( 88 (	070 95 .84 .75 .91 .97 .98	0.84 0.75 0.91 0.97 0.98	951009 0.5 0.4 0.6 0.8 0.8	05 95 59 17 39 32 35	0.43 0.34 0.50 0.59 0.61	953001 0.4 0.3 0.5 0.7 0.7	0 953 3 5 70 73	30020 0.23 0.10 0.36 0.53 0.58	9550	021 9 0.36 0.23 0.49 0.64 0.69	0.3 0.2 0.4 0.6 0.6	0 957 6 3 8 4 8	0.01 -0.11 0.14 0.31 0.36	957003 0.3 0.3 0.4 0.4 0.4	50 95 24 12 37 53 58	-0.03 -0.14 0.09 0.25 0.30
9: 9: 9: 9: 9: 9: 9:	340020 340030 360010 390010 410010 510010	9340020 1.00 0.99 0.94 0.92 0.63	934003 0.9 0.9 0.9 0.9 0.9 0.9	30 936 99 96 88 85 52	0010 9 0.99 0.96 1.00 0.98 0.96 0.96 0.73	0.94 0.94 0.98 0.98 1.00 1.00 0.85	941001 0.9 0.8 0.9 1.0 1.0 0.8	0 95 12 15 16 10 10 18	10010 0.63 0.52 0.73 0.85 0.88 1.00	951006 0.3 0.2 0.3 0.4 0.4 0.4	i0 95: 14 19 18 12 13 14	10063 0.83 0.74 0.90 0.96 0.98 0.95	95100 0.1 0.2 0.3 0.3 0.3 0.3	66         9510           74         (           66         (           80         (           87         (           88         (           86         (	070 95 .84 .75 .91 .97 .98 .95	0.84 0.75 0.91 0.97 0.98 0.95	951009 0.5 0.4 0.6 0.8 0.8 0.8	05 95 59 17 39 32 35 39	0.43 0.34 0.50 0.59 0.61 0.69	953001 0.4 0.3 0.5 0.7 0.7 0.9	0 953 3 41 5 70 73 6	30020 0.23 0.10 0.36 0.53 0.58 0.58 0.89	9550	021 9 0.36 0.23 0.49 0.64 0.69 0.94	0.3 0.2 0.4 0.6 0.6 0.9	0 957 6 3 8 4 8 4	0.01 -0.11 0.14 0.31 0.36 0.73	957003 0.3 0.4 0.4 0.4 0.4 0.4	50 95 24 12 37 53 58 87	-0.03 -0.14 0.09 0.25 0.30 0.66
9: 9: 9: 9: 9: 9: 9:	340020 340030 360010 390010 410010 510010 510060	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34	93400: 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	30 936 19 10 16 18 15 12 29	0010 9 0.99 0.96 1.00 0.98 0.96 0.73 0.38	0.390010 0.94 0.88 0.98 1.00 1.00 0.85 0.42	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4	0 95 12 15 16 10 10 18 13	10010 0.63 0.52 0.73 0.85 0.88 1.00 0.44	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 1.0	60 95 14 19 18 12 13 14 10	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45	95100 0. 0. 0. 0. 0. 0. 0. 0.	66         9510           74         (           66         (           80         (           87         (           88         (           86         (           45         (	070 95 .84 .75 .91 .97 .98 .95 .44	0.84 0.75 0.91 0.97 0.98 0.95 0.45	951009 0.5 0.4 0.6 0.8 0.8 0.8 0.9	05 95 59 17 59 52 55 99 13	0.43 0.34 0.50 0.59 0.61 0.69 0.29	953001 0.4 0.3 0.5 0.7 0.7 0.9 0.4	0 953 3 5 70 73 6 1	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35	9550	021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39	0.3 0.2 0.4 0.6 0.6 0.9 0.3	0 957 6 3 8 4 8 4 8 4 9	0040 0.01 -0.11 0.14 0.31 0.36 0.73 0.26	957003 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	50 95 24 12 37 53 58 87 35	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24
9: 9: 9: 9: 9: 9: 9: 9: 9:	340020 340030 360010 390010 410010 510010 510060 510063	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34 0.83	93400: 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	80 936 99 00 66 88 85 52 29 74	0010 9 0.99 0.96 1.00 0.98 0.96 0.73 0.38 0.90	0.94 0.94 0.88 0.98 1.00 1.00 0.85 0.42 0.96	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9	0 95 12 15 16 10 10 18 13 18	10010 0.63 0.52 0.73 0.85 0.88 1.00 0.44 0.95	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 1.0 0.4	i0 95: i4 i8 i8 i2 i3 i4 i0 i5	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45 1.00	95100 0.1 0.3 0.3 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	66         9510           74         (           66         (           80         (           87         (           88         (           86         (           45         (           90         1	070 95 .84 .75 .91 .97 .98 .95 .44 .00	0.84 0.75 0.91 0.97 0.98 0.95 0.45 1.00	951009 0.5 0.4 0.6 0.8 0.8 0.9 0.4 0.4 0.9	95 95 59 17 39 32 35 99 13 33	0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65	953001 0.4 0.3 0.5 0.7 0.7 0.9 0.4 0.8	0 95: 3 1 5 70 3 6 1 4	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71	9550	021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80	057001 0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8	0 957 6 3 8 4 4 9 0	0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49	957003 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	50 95 24 12 37 53 58 87 35 69	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42
9; 9; 9; 9; 9; 9; 9; 9; 9;	340020 340030 360010 390010 410010 510010 510060 510063 510066	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34 0.83 0.74	93400: 0.9 0.9 0.9 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1	80 936 99 90 96 98 95 52 99 74 96 96 97 4 96 97 97 97 97 97 97 97 97 97 97	0010 9 0.99 0.96 1.00 0.98 0.96 0.73 0.38 0.90 0.80	0.94 0.98 0.98 1.00 1.00 0.85 0.42 0.96 0.87	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9 0.8	0 95 12 15 16 10 10 18 13 18 18 18 18	10010 0.63 0.52 0.73 0.85 0.88 1.00 0.44 0.95 0.86	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 1.0 0.4 0.4	60 95 14 19 18 12 13 14 10 15 15	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45 1.00 0.90	95100 0. 0. 0. 0. 0. 0. 0. 0. 0. 1.	66         9510           74         0           66         0           80         0           87         0           88         0           86         0           45         0           90         1           00         0	070 95 .84 .75 .91 .97 .98 .95 .44 .00 .90	0.84 0.75 0.91 0.97 0.98 0.95 0.45 1.00 0.90	951009 0.5 0.4 0.6 0.8 0.8 0.9 0.4 0.4 0.9 0.8	95 95 59 17 39 32 35 99 13 34	0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65 0.58	953001 0.4 0.3 0.5 0.7 0.7 0.9 0.4 0.8 0.7	0 95: 3 5 70 3 6 11 44 7	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71 0.65	9550	021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80 0.73	057001 0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8 0.7	0 957 6 3 8 4 4 8 9 9 0 3	0040 0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49 0.45	957003 0.1 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	50 95 24 12 37 53 58 87 35 87 35 69 64	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42 0.39
9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9:	340020 340030 360010 390010 410010 510060 510063 510066 510070	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34 0.83 0.74 0.84	93400 0.9 1.0 0.9 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	80 936 99 90 96 88 85 52 29 74 66 75	0010 § 0.99 0.96 1.00 0.98 0.96 0.73 0.38 0.90 0.80 0.91	0.94 0.94 0.88 0.98 1.00 1.00 0.85 0.42 0.96 0.87 0.97	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9 0.8 0.9 0.8 0.9	0 95 12 15 16 10 10 18 13 18 18 18 18 18 18	10010 0.63 0.52 0.73 0.85 0.88 1.00 0.44 0.95 0.86 0.95	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	i0 95 i4 i2 i3 i4 i2 i3 i4 i5 i5 i4	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45 1.00 0.90 1.00	95100 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	66         9510           74         0           66         0           80         0           87         0           88         0           86         0           45         0           90         1           90         1	170         95           .84         .75           .91         .97           .98         .95           .44         .00           .90         .00	0.84 0.75 0.91 0.97 0.98 0.95 0.45 1.00 0.90 1.00	951009 0.5 0.4 0.6 0.8 0.5 0.5 0.4 0.4 0.5 0.5 0.5 0.5	95 95 59 47 39 32 35 99 43 33 34 92	0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65 0.58 0.65	953001 0.4 0.3 0.5 0.7 0.7 0.7 0.9 0.4 0.8 0.7 0.8	0 95: 3 5 7 6 1 7 4 4 4	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71 0.65 0.71		021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80 0.73 0.80	057001) 0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8 0.7 0.8	0 957 6 3 8 4 4 8 9 0 3 0	0.040 0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49 0.45 0.50	957003 0.: 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	50 95 24 12 37 53 58 87 35 69 64 70	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42 0.39 0.44
9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9:	340020 340030 360010 390010 510010 510060 510063 510066 510070 510075	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34 0.83 0.74 0.84 0.84	934003 934003 9 0.9 9 0.	80 936 99 90 96 88 85 52 29 74 66 75 75	0010 9 0.99 0.96 0.98 0.96 0.73 0.38 0.90 0.80 0.91 0.91	0390010 0.94 0.88 0.98 1.00 1.00 0.85 0.42 0.96 0.87 0.97 0.97	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9 0.8 0.9 0.9 0.9 0.9	0 95 12 15 16 10 10 18 13 18 18 18 18 18 18 18 18 18 18	10010 0.63 0.52 0.73 0.85 0.88 1.00 0.44 0.95 0.86 0.95 0.95	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	60 95 84 89 88 12 13 14 15 15 14 15	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45 1.00 0.90 1.00 1.00	95100 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	66         9510           74         (           66         (           80         (           87         (           88         (           88         (           90         1           90         1           90         1	170         95           .84         .75           .91         .97           .98         .95           .44         .00           .90         .00           .00         .00	0.84 0.75 0.91 0.97 0.98 0.95 0.45 1.00 0.90 1.00 1.00	951009 0.5 0.4 0.6 0.8 0.8 0.8 0.9 0.4 0.9 0.8 0.8 0.9 0.8 0.8 0.8 0.8 0.9 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	95 95 59 17 39 32 35 19 13 13 33 34 92 93	0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65 0.58 0.65 0.65	953001 0.4 0.3 0.5 0.7 0.7 0.7 0.9 0.4 0.8 0.7 0.8 0.8 0.8	0 95: 3 5 7 6 1 7 7 4 4 4 4 4	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71 0.65 0.71 0.71 0.71		021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80 0.73 0.80 0.80 0.80	057001) 0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8 0.7 0.8 0.8 0.7 0.8 0.8	0 957 6 3 8 4 4 9 0 3 0 0 0	0.040 0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49 0.45 0.50 0.50	957003 0.: 0.: 0.: 0.: 0.: 0.: 0.: 0.: 0.: 0.:	50 95 24 12 37 53 58 87 35 87 35 69 64 70 70	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42 0.39 0.44 0.44
9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9	340020 340030 360010 390010 510010 510060 510063 510066 510070 510075 510095	9340020 1.00 0.99 0.94 0.92 0.63 0.34 0.83 0.74 0.84 0.84 0.84	934003 934003 1.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0	80 936 99 90 96 88 85 52 29 74 66 75 75 75	0010 9 0.99 0.96 1.00 0.98 0.96 0.73 0.38 0.90 0.80 0.91 0.91 0.91 0.69	0390010 0.94 0.88 0.98 1.00 0.85 0.42 0.96 0.87 0.97 0.97 0.82	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9 0.8 0.9 0.9 0.9 0.9 0.8	0 95 12 15 16 10 10 18 18 18 18 18 18 18 18 18 18	10010 0.63 0.52 0.73 0.85 0.88 1.00 0.44 0.95 0.86 0.95 0.95 0.99	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	i0 95 i4 i2 i3 i4 i5 i5 i4 i5 i3 i4 i5 i3 i4 i5 i3 i4 i5 i3 i5 i4 i5 i5 i5 i6 i6 i7 i7 i8 i8 i8 i8 i8 i8 i8 i8 i8 i8	10063 0.83 0.74 0.90 0.96 0.95 0.45 1.00 0.90 1.00 1.00 0.93	95100 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	74         0           74         0           74         0           74         0           74         0           76         0           88         0           88         0           90         1           90         1           90         1           90         1           90         1           90         1	170         95           .84         .75           .91         .97           .98         .95           .44         .00           .90         .00           .00         .92	0.84 0.75 0.91 0.97 0.98 0.95 0.45 1.00 0.90 1.00 1.00 0.93	951009 0.5 0.4 0.6 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	95 95 59 17 39 32 35 99 13 33 34 92 33 90 0	0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65 0.58 0.65 0.65 0.65 0.65	953001 0.4 0.3 0.5 0.7 0.7 0.9 0.4 0.8 0.7 0.8 0.8 0.8 0.8 0.9	0 95: 3 5 70 3 66 11 44 44 44 47 7	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71 0.65 0.71 0.71 0.71 0.91		021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80 0.73 0.80 0.80 0.80 0.96	057001) 0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8 0.7 0.8 0.8 0.7 0.8 0.9 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.3 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0 957 6 3 8 4 4 9 0 3 0 0 5	0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49 0.45 0.50 0.50 0.50 0.76	957003 0.: 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.4 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	50 95 24 12 37 53 58 87 35 87 35 69 64 70 70 90	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42 0.39 0.44 0.44 0.44
9; 9; 9; 9; 9; 9; 9; 9; 9; 9; 9; 9; 9;	340020 340030 360010 390010 510010 510060 510063 510066 510070 510075 510095 510132	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34 0.83 0.74 0.8	934003 934003 90.0.9 90.00000000	80 936 99 90 96 88 85 52 29 74 66 75 75 75 17 84	0010         9           0.99         0.96           1.00         0.98           0.96         0.73           0.38         0.90           0.80         0.91           0.91         0.91           0.50         0.50	0390010 0.94 0.88 0.98 1.00 0.85 0.42 0.96 0.87 0.97 0.97 0.82 0.59	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9 0.8 0.9 0.8 0.9 0.9 0.9 0.9 0.9 0.9	0 95 12 15 16 10 10 18 18 18 18 18 18 18 18 18 18	0.63           0.52           0.73           0.85           0.88           1.00           0.44           0.95           0.86           0.95           0.95           0.95           0.95           0.95           0.95           0.90	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	i0 95: 44 29 18 12 13 14 15 15 15 14 15 13 29	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45 1.00 0.90 1.00 1.00 0.93 0.65	951000 0.1 0.3 0.3 0.3 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	666         9510           774         (           666         (           680         (           688         (           688         (           690         1           000         (           090         1           190         1           884         (           685         (           686         (           687         (           688         (           690         1           190         1           884         (           658         (	070         95           .84         .75           .91         .97           .98         .95           .44         .00           .90         .00           .00         .92           .65         .65	0.84           0.75           0.91           0.97           0.98           0.95           0.45           1.00           0.90           1.00           0.93           0.65	951009 0.5 0.4 0.6 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	95 95 99 17 17 19 12 13 13 13 13 13 13 13 13 13 13	0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65 0.58 0.65 0.65 0.65 0.68 1.00	953001 0.4 0.3 0.5 0.7 0.7 0.9 0.4 0.8 0.7 0.8 0.8 0.8 0.8 0.9 0.6	0 95: 3 3 5 70 3 6 6 11 4 4 4 4 4 4 7 7 4 4 4 4 7 7 4 4	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71 0.65 0.71 0.71 0.71 0.91 0.61		021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80 0.73 0.80 0.80 0.96 0.65	0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8 0.7 0.8 0.7 0.8 0.8 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.8 0.9 0.2 0.2 0.4 0.4 0.4 0.5 0.2 0.4 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	0 957 6 3 8 8 4 4 9 9 0 3 0 0 5 4	0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49 0.45 0.50 0.50 0.50 0.76 0.49	957003 0.: 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	50 95 24 12 37 53 58 87 35 69 64 70 70 90 58	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42 0.39 0.44 0.44 0.44 0.49 0.43
9; 9; 9; 9; 9; 9; 9; 9; 9; 9; 9; 9; 9; 9	340020 340030 360010 390010 510010 510060 510063 510066 510070 510075 510075 510095 510132 530010	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34 0.83 0.74 0.84 0.84 0.59 0.43 0.43	934003 934003 900,9340003 900,934000 900,934000 900,934000 900,934000 900,934000 900,934000 900,934000 900,934000 900,934000 900,934000 900,934000000000000000000000000000000000	80 936 99 90 96 88 85 52 29 75 75 75 75 75 84 81	0010         9           0.99         0.96           1.00         0.98           0.96         0.73           0.38         0.90           0.80         0.91           0.91         0.91           0.50         0.55	0.94 0.94 0.88 0.98 1.00 1.00 0.85 0.42 0.96 0.87 0.97 0.97 0.87 0.97 0.59 0.70	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9 0.8 0.9 0.9 0.9 0.9 0.8 0.6 0.7	0 95 12 15 16 10 10 10 18 13 18 18 18 18 18 18 18 18 18 18	10010 0.63 0.52 0.73 0.85 0.85 1.00 0.44 0.95 0.95 0.95 0.99 0.69 0.96	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	i0 95: 44 29 18 12 13 14 15 15 15 14 15 13 29 11	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45 1.00 0.90 1.00 1.00 0.93 0.65 0.84	951000 0.1 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	74         0           74         0           66         0           80         0           88         0           888         0           900         1	070         95           .84         .75           .91         .97           .98         .95           .44         .00           .90         .00           .00         .92           .65         .84	$\begin{array}{c} 0.84\\ 0.75\\ 0.91\\ 0.97\\ 0.98\\ 0.95\\ 0.45\\ 1.00\\ 0.90\\ 1.00\\ 1.00\\ 0.93\\ 0.65\\ 0.84 \end{array}$	951009 0.5 0.4 0.6 0.8 0.8 0.8 0.4 0.4 0.4 0.4 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	95 95 99 17 39 32 35 99 13 33 34 92 93 90 13 90 13 92 93 93 94 95 95 95 95 95 95 95 95 95 95	0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65 0.58 0.65 0.65 0.65 0.68 1.00 0.64	953001 0.4 0.3 0.5 0.7 0.7 0.7 0.9 0.4 0.8 0.7 0.8 0.8 0.8 0.9 0.6 0.10	0 95: 3 5 5 70 3 6 11 4 4 7 4 4 7 4 4 10 7 4 10 10 10 10 10 10 10 10 10 10	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71 0.65 0.71 0.71 0.71 0.91 0.61 0.96		021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80 0.73 0.80 0.80 0.80 0.96 0.65 0.98	0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8 0.7 0.8 0.7 0.8 0.8 0.8 0.9 0.6 0.9	0 957 6 3 8 8 4 8 4 9 9 0 3 0 0 3 0 0 5 4 4 8	0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49 0.45 0.50 0.50 0.50 0.50 0.76 0.49 0.85	957003 0.: 0.3 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	50 95 24 12 37 53 58 87 35 69 64 70 70 90 58 95	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42 0.39 0.44 0.44 0.44 0.43 0.43 0.80
9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9: 9	340020 340030 360010 390010 510010 510063 510063 510063 510075 510075 510075 510075 510075 510075 510032 530010 530020	9340020 1.00 0.99 0.99 0.94 0.92 0.63 0.34 0.83 0.74 0.84 0.84 0.59 0.43 0.43 0.43 0.43	934003 934003 90.9 90.9 90.9 90.9 90.9 90.9 90.9 9	80 936 99 90 96 88 85 52 29 74 66 75 75 75 75 75 75 75 75 75 75 75 75 75	0010         9           0.99         0.96           1.00         0.98           0.96         0.73           0.38         0.90           0.80         0.91           0.91         0.50           0.55         0.36	0.94 0.94 0.88 0.98 1.00 1.00 0.85 0.42 0.96 0.87 0.97 0.97 0.82 0.57 0.53	941001 0.9 0.8 0.9 1.0 1.0 0.8 0.4 0.9 0.8 0.9 0.9 0.9 0.9 0.8 0.6 0.7 0.5	0 95 12 15 16 10 10 10 18 13 18 18 18 18 18 18 18 18 18 18	10010 0.63 0.52 0.73 0.85 0.88 1.00 0.44 0.95 0.95 0.95 0.99 0.69 0.96 0.89	951006 0.3 0.2 0.3 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	i0 95: 14 19 18 12 13 13 14 10 15 15 15 14 15 13 19 11 15 15 15 13 19 15 15 15 15 15 15 15 15 15 15	10063 0.83 0.74 0.90 0.96 0.98 0.95 0.45 1.00 0.90 1.00 1.00 0.93 0.65 0.84 0.71	951000 0.1 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	666         9510           774         (           666         (           880         (           887         (           888         (           888         (           900         11           900         11           900         11           900         12           900         13           900         14	070         95           .84         .75           .91         .97           .98         .95           .44         .00           .90         .00           .92         .65           .84         .71	0.84 0.75 0.91 0.97 0.98 0.95 0.45 1.00 0.90 1.00 1.00 0.93 0.65 0.84 0.71	951009 0.5 0.4 0.4 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	05 95 59 17 59 12 55 59 13 13 13 13 13 13 13 10 15 16 17 17 17 17 17 17 17 17 17 17	10132 0.43 0.34 0.50 0.59 0.61 0.69 0.29 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.65 0.64 0.00 0.64 0.61	953001 0.4 0.3 0.5 0.7 0.7 0.9 0.4 0.8 0.7 0.8 0.8 0.9 0.6 1.0 0.9 0.9	0 95: 3 5 5 70 3 6 11 4 4 7 4 4 17 4 10 10 10 10 10 11 10 10 10 10	30020 0.23 0.10 0.36 0.53 0.58 0.89 0.35 0.71 0.65 0.71 0.71 0.91 0.61 0.96 1.00		021 9 0.36 0.23 0.49 0.64 0.69 0.94 0.39 0.80 0.73 0.80 0.80 0.80 0.96 0.65 0.98 0.99	0570010 0.3 0.2 0.4 0.6 0.6 0.9 0.3 0.8 0.7 0.8 0.8 0.9 0.6 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0 957 6 3 8 4 4 8 9 0 0 3 0 0 0 5 4 4 8 9 9 0 0 5 4 9 9	0.01 -0.11 0.14 0.31 0.36 0.73 0.26 0.49 0.45 0.50 0.50 0.50 0.50 0.76 0.49 0.85 0.93	957003 0.: 0.: 0.: 0.: 0.: 0.: 0.: 0.: 0.: 0.:	50 95 24 12 37 53 58 87 35 87 35 69 64 70 70 90 58 95 98	-0.03 -0.14 0.09 0.25 0.30 0.66 0.24 0.42 0.39 0.44 0.42 0.39 0.44 0.43 0.44 0.69 0.43 0.80 0.90
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